

Tutorial 6

1) (a) for a cyclic process, I. law states that $\oint \delta Q = \oint \delta W$



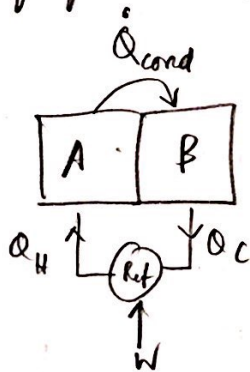
$$\oint_{\text{cycle}} \delta Q = \oint_{\text{cycle}} T ds = \text{area in the cycle}$$

$$\oint \delta W = \oint P dV = \text{area in the PV diagram}$$

\therefore the two areas are equal!

(b) it is true for any cycle so it is true for refrigeration cycle as well

2)



$$\dot{Q}_{\text{cond}} = -KA \frac{dT}{dx} = \frac{KA(T_A - T_B)}{S_u}$$

for steady state,

$$\dot{Q}_{\text{cond}} = \dot{Q}_C$$

for minimum work

$$\text{reversible refrigerator} \Rightarrow \dot{Q}_H = \frac{\dot{Q}_C}{T_B} T_A$$


$$\dot{W} = \dot{Q}_H - \dot{Q}_C$$

$$\begin{aligned}\therefore \dot{W} &= \dot{Q}_H - \dot{Q}_C \\ &= \dot{Q}_C \left(\frac{T_A}{T_C} - 1 \right) = \frac{\dot{Q}_{\text{cond}}}{(\text{COP})_{\text{ref}}}\end{aligned}$$

$$\dot{W} = \frac{K_A(T_A - T_B)}{(\text{COP})_{\text{ref}}}$$

$$\Delta S = \Delta S_A + \Delta S_B + \cancel{\Delta S_{\text{ref}}} = \frac{\dot{Q}_H}{T_A} - \frac{\dot{Q}_C}{T_B} - \frac{\dot{Q}_{\text{cond}}}{T_A} + \frac{\dot{Q}_{\text{cond}}}{T_B}$$

$$= \dot{Q}_{\text{cond}} \left[\frac{1}{T_B} - \frac{1}{T_A} \right] = \frac{\dot{W}}{T_A}$$

3.  $V = 0.2 \text{ m}^3$ 25°C 1 bar
 water $m = \frac{1}{2} \text{ kg}$
 2 gms evaporated

$$\eta_{\text{air}} = \frac{PV}{RT} = \frac{10^5 \times 0.2}{8.314 \times 288} = 8.07 \text{ moles}$$

$$m_{\text{air}} = 28.8 \times 10^{-3} \times 8.07 = 0.232 \text{ kg}$$

$$\eta_w = \frac{2 \times 10^{-3}}{18} = 0.111 \text{ mol}$$

$$X_w = \frac{\eta_w}{\eta_a + \eta_w} = \frac{0.111}{8.07 + 0.11} = 0.013$$

$$Y_w = \frac{m_w}{m_a + m_w} = \frac{2 \times 10^{-3}}{2 \times 10^{-3} + 0.232} = 0.00854$$

4)

	mass %	
CH_4	= 58%	$C_{p\text{CH}_4} = 35.06 \text{ kJ/kmol K}$
H_2	= 18%	$C_{p\text{H}_2} = 29.01$ "
N_2	= 10%	$C_{p\text{N}_2} = 28.87$ "
CO	= 14%	$C_{p\text{CO}} = 28.88$ "

$$(a) \frac{1}{M_{w,m}} = \sum_i \frac{Y_i}{M_{wi}} = \frac{0.58}{16} + \frac{0.18}{2} + \frac{0.1}{28} + \frac{0.14}{28} = 0.135$$

$$(b) R_m = \frac{8.314}{7.42} = 1120 \text{ J/kgK}$$

$$(c) C_{p,m} = \sum_i Y_i C_{pi} = \sum_i Y_i \hat{C}_{pi}$$

$$= \frac{0.58}{16} \times 35.06 + \frac{0.18}{2} \times 29.01 + \frac{0.1}{28} \times 28.87$$

$$+ \frac{0.14}{28} \times 28.88 = 4.129 \frac{\text{kJ}}{\text{kgK}}$$

$$C_{v,m} = C_{p,m} - R_m = 4.129 - 1.12$$

$$= 3.009 \text{ kJ/kgK}$$

5.

①	②	③
0.1 m ³	0.2 m ³	0.05 m ³
H ₂	N ₂	CO ₂

$$V_{\text{total}} = 0.35 \text{ m}^3$$

$$P = 2 \text{ bar} \quad T = 13^\circ\text{C} = 286 \text{ K}$$

mixing: $n_{\text{H}_2} = \frac{PV_{\text{H}_2}}{RT} = \frac{2 \times 10^5 \times 0.1}{8.314 \times 286} = 8.41 \text{ moles}$

$$n_{\text{N}_2} = \frac{2 \times 10^5 \times 0.2}{8.314 \times 286} = 16.82 \text{ moles}$$

$$n_{\text{CO}_2} = \frac{2 \times 10^5 \times 0.05}{8.314 \times 286} = 4.205 \text{ moles}$$

$$X_{H_2} = \frac{8.41}{29.44} = 0.286$$

$$X_{N_2} = 0.572$$

$$X_{CO_2} = 0.143$$

$$a) M_m = \sum X_i M_i$$

$$= 0.286 \times 2 + 0.572 \times 28$$

$$+ 0.143 \times 44$$

$$= 22.88 \text{ kg/kmol}$$

$$b) P_m = \frac{8.314}{22.88} = 363.4 \frac{\text{J}}{\text{kgK}}$$

$$c) P_i = X_i P \rightarrow P_{H_2} = 0.572 \text{ bar}; P_{N_2} = 1.144 \text{ bar}; P_{CO_2} = 0.286 \text{ bar}$$

$$d) C_{p_{mix}} = \sum_i X_i \hat{C}_{p_i} = \sum_i X_i (C_{p_i} N_i)$$

$$= 0.286 \times 2 \times 14.235 + 0.572 \times 28 \times 1.039$$

$$+ 0.143 \times 0.828 \times 44$$

$$= 29.99 \frac{\text{kJ}}{\text{kmol K}}$$

$$C_{v_{mix}} = C_{p_{mix}} - P_{mix} = 29.99 - 8.314 = 21.676 \frac{\text{kJ}}{\text{kmol K}}$$

$$\gamma = 1.384$$

e) each gas occupies the full volume during mixing through free expansion

$$\Delta S = C_v \ln\left(\frac{T_2}{T_1}\right) + R \ln\left(\frac{V_2}{V_1}\right)$$

$$\Delta S_{H_2} = \frac{8.314 \times 10^3}{2} \ln\left(\frac{0.35}{2}\right) = 5.21 \frac{\text{kJ}}{\text{kg K}}$$

$$\Delta S_{N_2} = \frac{8.314}{28} \ln\left(\frac{0.35}{0.2}\right) = 0.166 \frac{\text{kJ}}{\text{kg K}}$$

$$\Delta S_{CO_2} = \frac{8.314}{44} \ln\left(\frac{0.35}{0.05}\right) = 0.367 \frac{\text{kJ}}{\text{kg K}}$$

$$\Delta S_{\text{mix}} = \left[0.286 \times 2 \times 5.21 + 0.572 \times 28 \times 0.166 + 0.143 \times 44 \times 0.367 \right] \frac{1}{22.88}$$

5.

$$= 0.3474 \frac{\text{kJ}}{\text{kg K}}$$

Compression:

$$P V^{1.2} = \text{const.}$$

$$\text{Work for } P V^n = \text{const process: } W = \int_1^2 P dV = \frac{P_1 V_1 - P_2 V_2}{n-1}$$

$$V_2 = \left(\frac{P_1}{P_2} \right)^{\frac{1}{1.2}} V_1$$

$$W = \left[\frac{2 \times 0.35 - 6 \times 0.14}{0.2} \right] \times 10^5 = -70 \text{ kJ}$$

$$= \left(\frac{2}{6} \right)^{\frac{1}{1.2}} \times 0.35 = 0.14 \text{ m}^3$$

$$T_2 = \frac{P_2 V_2}{nR} = \frac{6 \times 10^5 \times 0.14}{29.44 \times 8.314} = 343.4 \text{ K}$$

$$\Delta Q = \Delta E + \Delta W = 21.676 \frac{\text{J}}{\text{mol K}} \times 29.44 (343.2 - 286) - 70$$

$$= -33.5 \text{ kJ}$$

$$g) \Delta S = N \left(\hat{C}_p \ln \left(\frac{T_2}{T_1} \right) - \hat{R} \ln \left(\frac{P_2}{P_1} \right) \right)$$

$$= 29.44 \left[29.99 \ln \left(\frac{343.2}{286} \right) - 8.314 \ln \left(\frac{6}{2} \right) \right] = -107.9 \frac{\text{J}}{\text{K}}$$