

Lecture 9.

Polariser: (Lecture 7)

$$\begin{pmatrix} A'_x \\ A'_y \end{pmatrix} = \begin{pmatrix} \cos^2 \theta & \sin \theta \cos \theta \\ \sin \theta \cos \theta & \sin^2 \theta \end{pmatrix} \begin{pmatrix} A_x \\ A_y \end{pmatrix}$$

A' ← emergent P_θ A ← incident

$$A' = P_\theta \cdot A$$

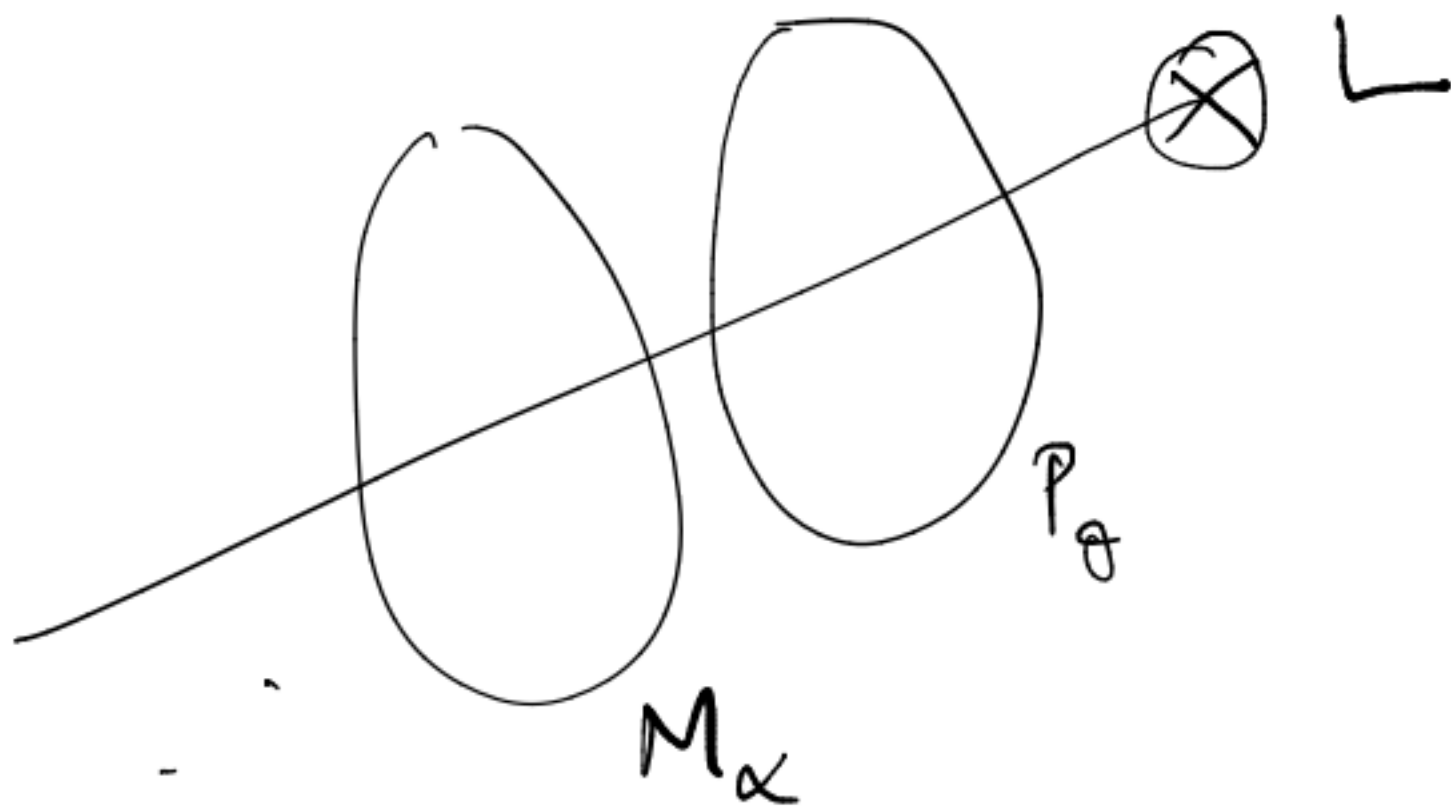
Birefringent plate (Lecture 8)

$$\begin{pmatrix} A'_x \\ A'_y \end{pmatrix} = \begin{pmatrix} \cos^2 \alpha + e^{i\delta} \sin^2 \alpha & (1 - e^{i\delta}) \sin \alpha \cos \alpha \\ (1 - e^{i\delta}) \sin \alpha \cos \alpha & \sin^2 \alpha + e^{i\delta} \cos^2 \alpha \end{pmatrix} \begin{pmatrix} A_x \\ A_y \end{pmatrix}$$

A' ← emergent M_α A ← incident

$$A' = M_\alpha \cdot A$$

An optical system =



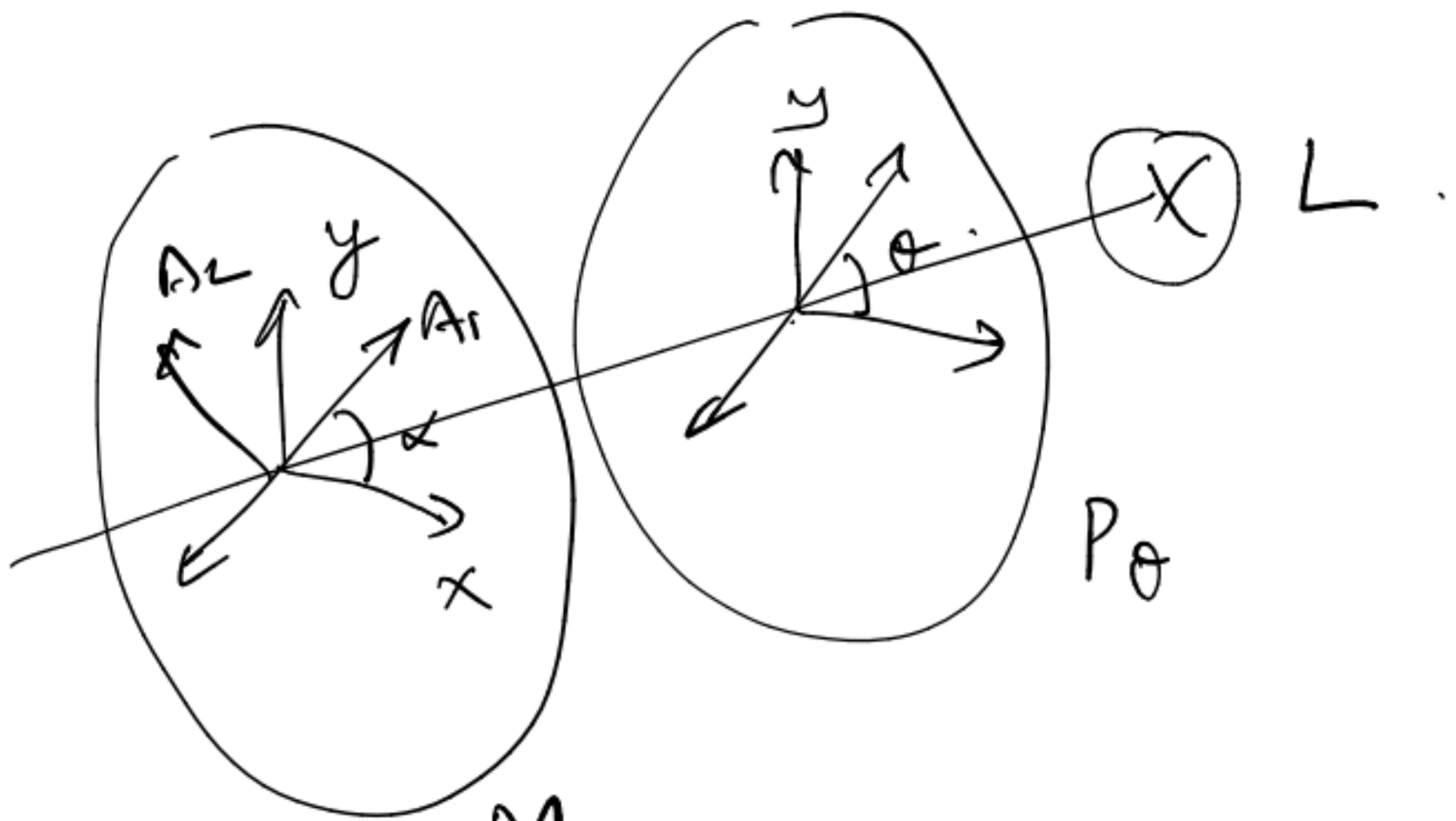
$$A' = M_\alpha P_\theta A$$

complex amplitudes of light from L.

emergent wave from the polarizer.

emergent light from the birefringent sheet

Optical system to produce
circularly polarised light:



For $D = \frac{\pi}{2}$ (Quarter wave plate) of the Birefringent sheet, we will get circularly polarised light, provided

OR $\theta = 0, \alpha \neq 0 \text{ or } \frac{\pi}{2}$
 $\theta = \frac{\pi}{2}, \alpha = (0, \text{ or } \frac{\pi}{2})$.

For circularly polarised light,
 recall. $\begin{pmatrix} A'_x \\ A'_y \end{pmatrix} = A \begin{pmatrix} 1 \\ \pm i \end{pmatrix}$... (1)

$$\begin{pmatrix} A'_x \\ A'_y \end{pmatrix} = \begin{pmatrix} 1 & \mp i \\ \mp i & 1 \end{pmatrix} \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} A_x \\ A_y \end{pmatrix}$$

↑
 Quarter wave
 plate

$$= \begin{pmatrix} \mp i \\ 1 \end{pmatrix} A_y$$

$$= \begin{pmatrix} \mp 1 \\ i \end{pmatrix} A_y \dots (2)$$

Compare (1) & (2) to see that a circularly polarised light beam

emerges from the quarter wave plate.

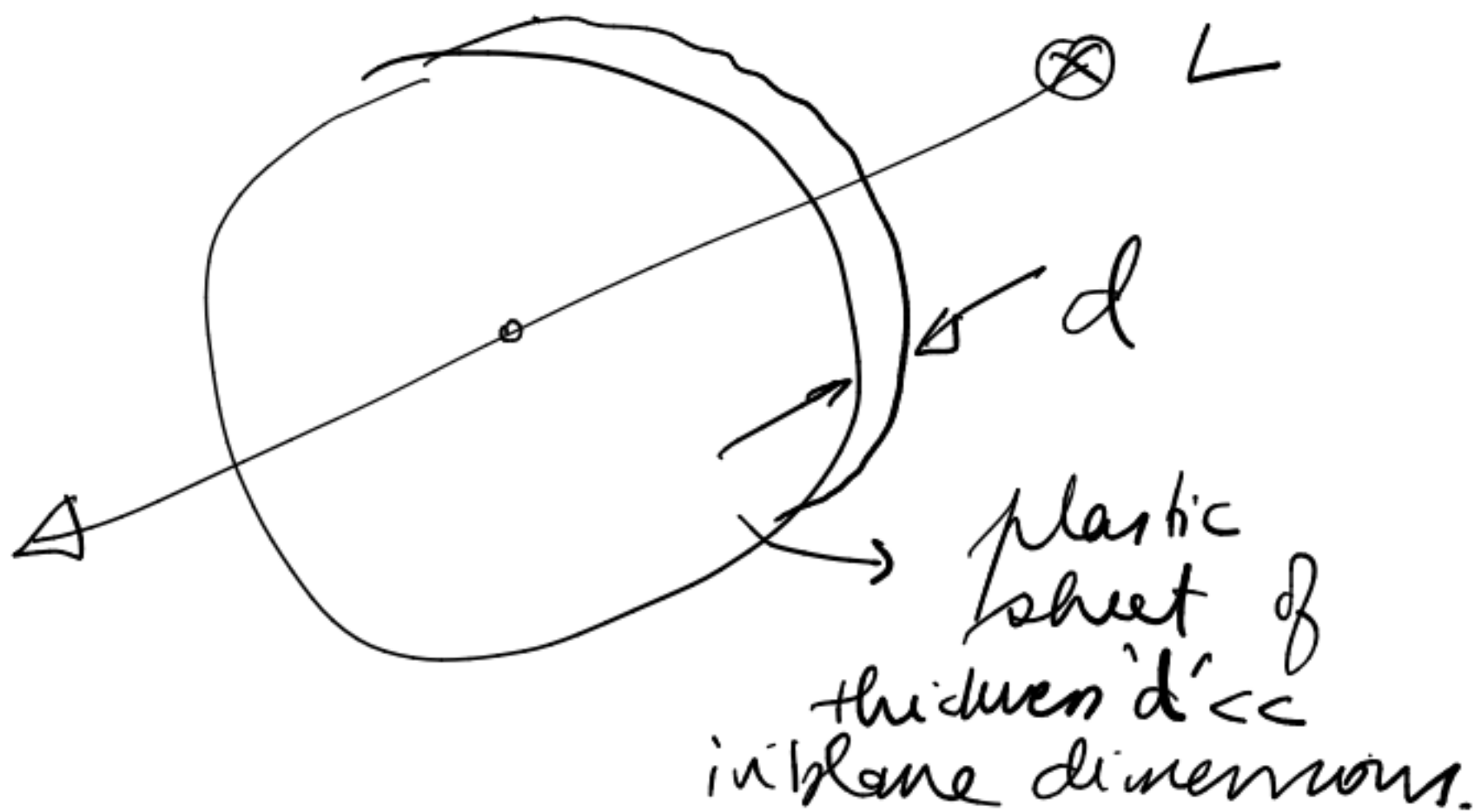
Elliptically polarised light

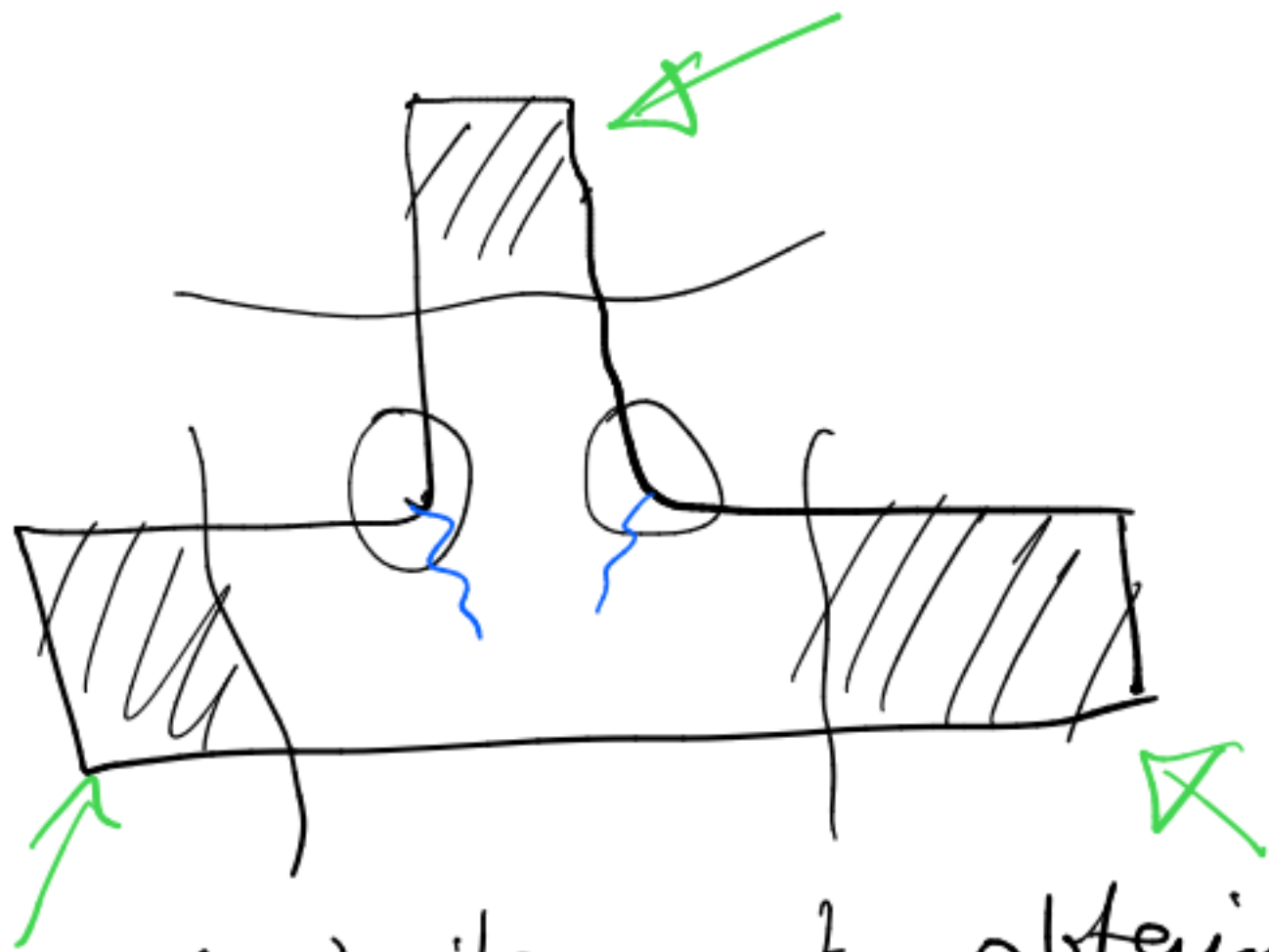
→ set $\alpha \neq 0$ or $\frac{\pi}{4}$ or $\frac{\pi}{2}$.

Refractive indices

of stressed transparent

materials





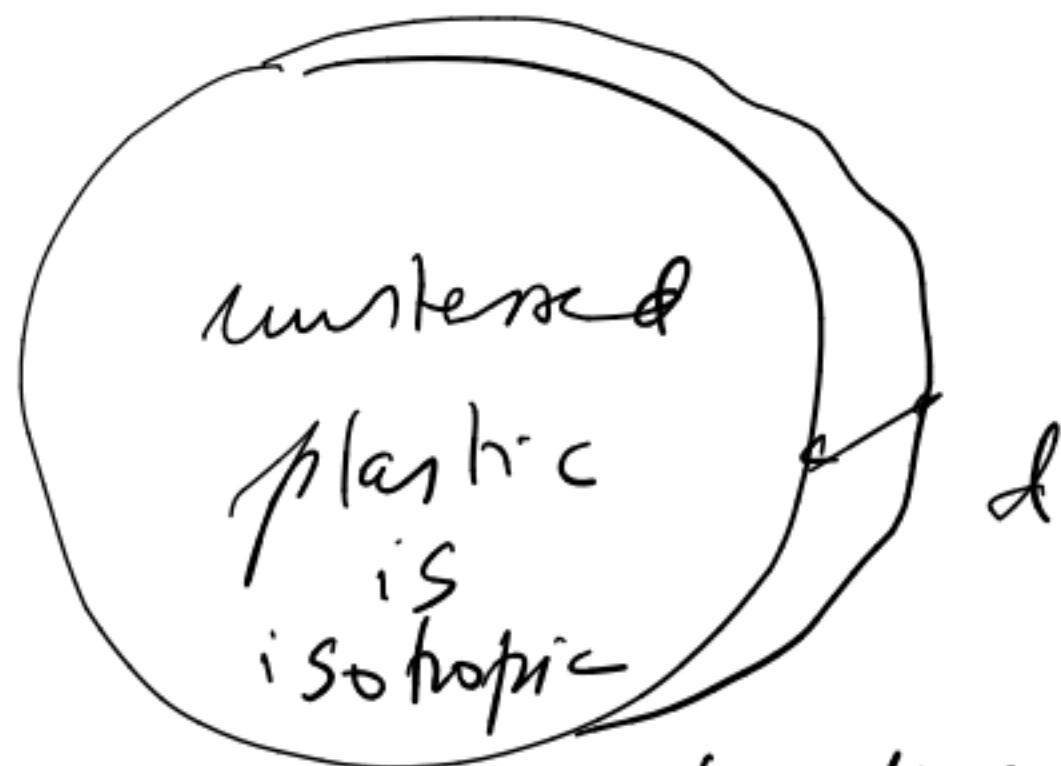
① Photoelasticity — to obtain critical stresses in non-slender components

② Photoelasticity is not used for this purpose anymore because FEM has totally replaced it.

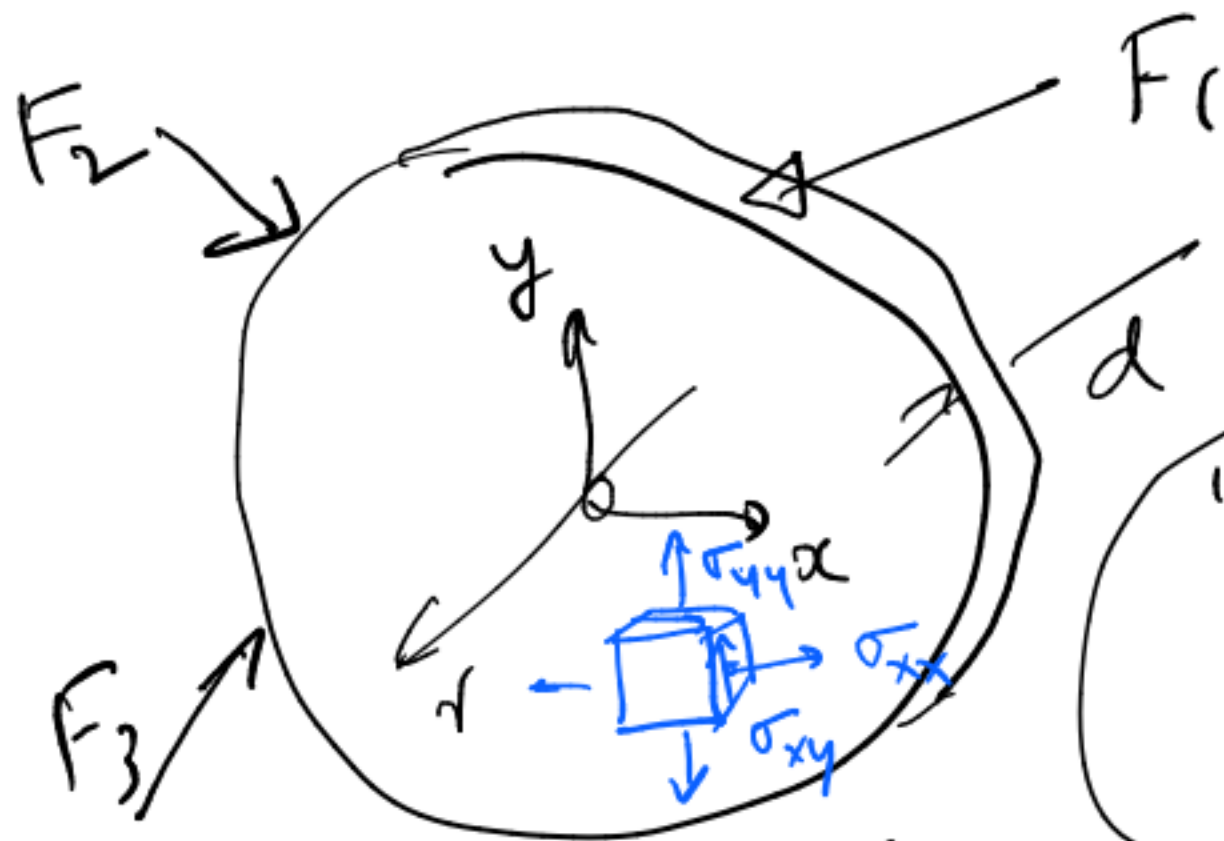
③ When photoelastic analysis was used, a scaled replica of the relevant structure would

be prepared in plastic, loaded,
photo elasticity would yield
stress values, these values
would be scaled to the
original component.

How does stress change the
refractive indices of thin
plastic sheets?



Let n_0 be its refractive index.



"plane stress"

Stressed plastic becomes optically anisotropic.

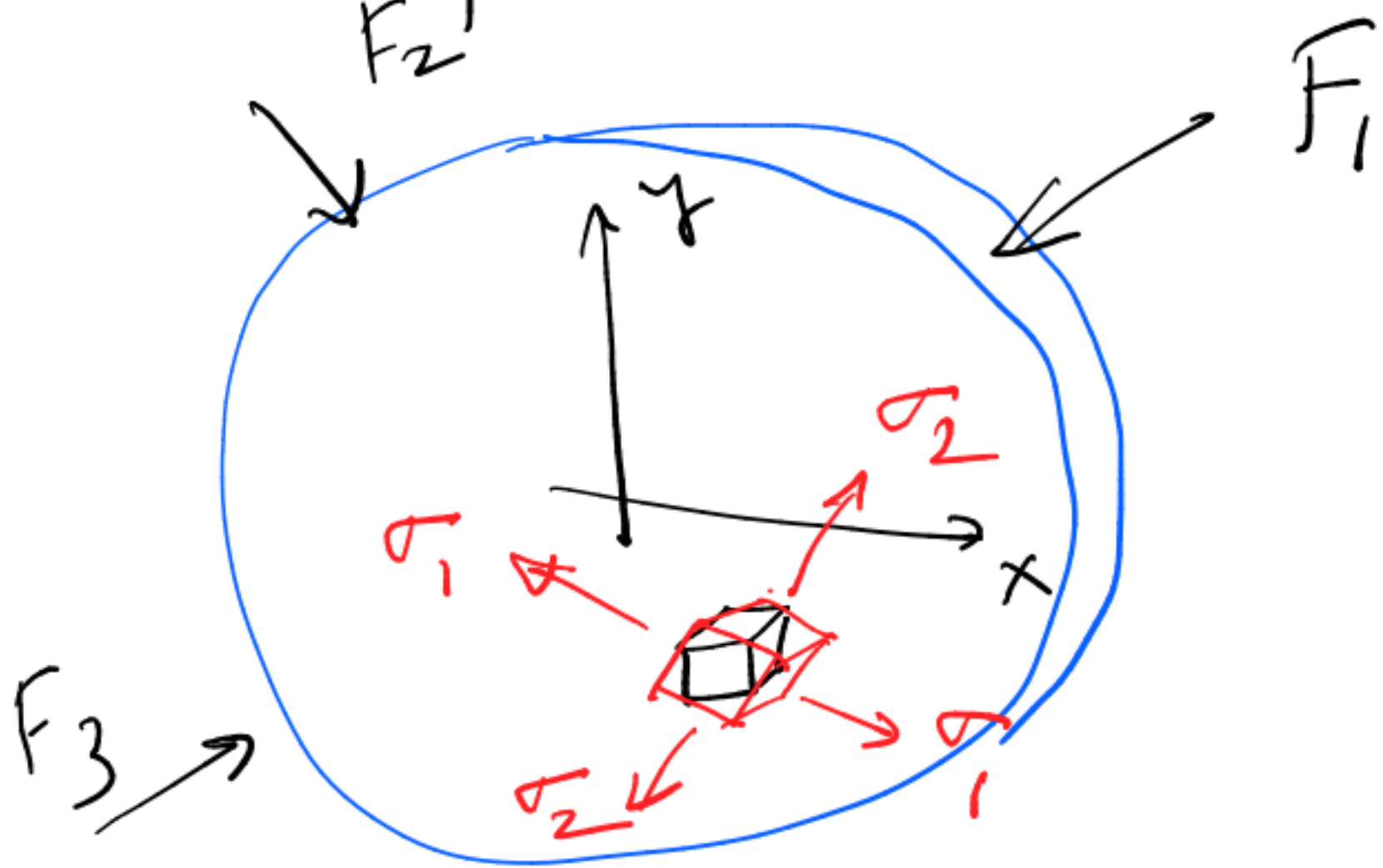
$$\begin{aligned} \sigma_{zz} &= 0 \\ \sigma_{zx} &= 0 \\ \sigma_{zy} &= 0. \end{aligned}$$

Optical anisotropy cannot depend on $\sigma_{xx}, \sigma_{yy}, \sigma_{xy}$

$$\begin{aligned} \sigma_{xx} &\neq 0 \\ \sigma_{yy} &\neq 0 \\ \sigma_{xy} &\neq 0 \end{aligned}$$

because x & y are dependant on the observer & not on the phenomenon of stress generate.

Optical anisotropy must depend only on the principal stresses & the principal directions developed @ each & every pt. in the plate.



red element aligned w/ σ_1, σ_2
 σ_1, σ_2 principal axes play
 the role of A_1, A_2 in the
 birefringent filter we studied earlier.

The light polarized along σ_1
& σ_2 experience different
refractive indices.

How?

Let $\sigma_1, \sigma_2, \sigma_3$ be the 3 principal
stresses @ a point.

Then,

Material constants

$$\begin{aligned} \text{(a)} \quad n_1 - n_0 &= c_1 \sigma_1 + c_2 (\sigma_2 + \sigma_3) \\ \text{(b)} \quad n_2 - n_0 &= c_1 \sigma_2 + c_2 (\sigma_3 + \sigma_1) \\ \text{(c)} \quad n_3 - n_0 &= c_1 \sigma_3 + c_2 (\sigma_1 + \sigma_2) \end{aligned}$$

n_0 = refractive index of the
unstressed state.

c_1, c_2 = stress-optic coefficients
= Material constants.

To eliminate no. do

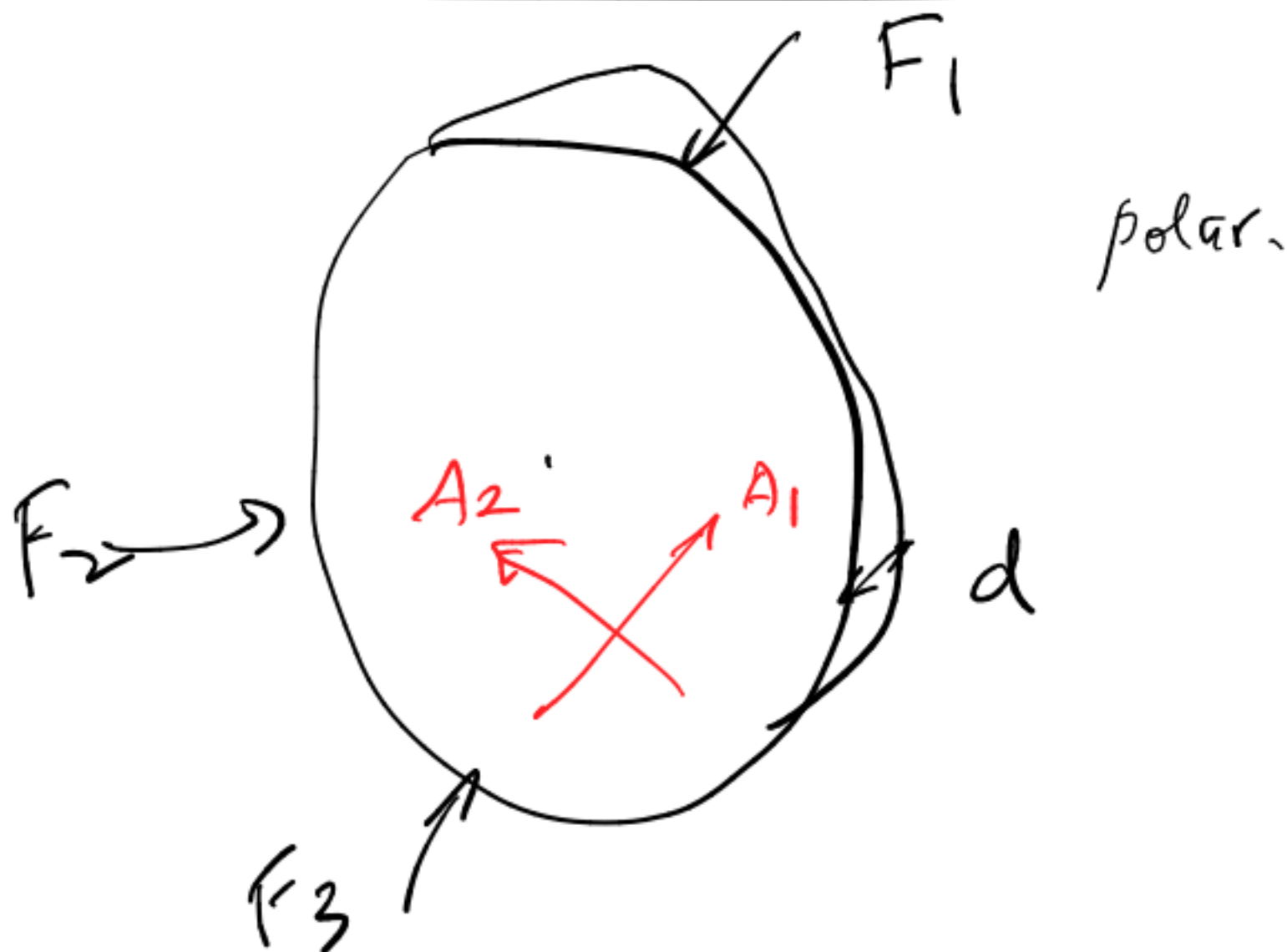
(a)-(b), (b)-(c), (c)-(a):

$$n_2 - n_1 = (\sigma_1 - \sigma_2) (c_2 - c_1)$$

$$n_3 - n_2 = (\sigma_2 - \sigma_3) (c_2 - c_1)$$

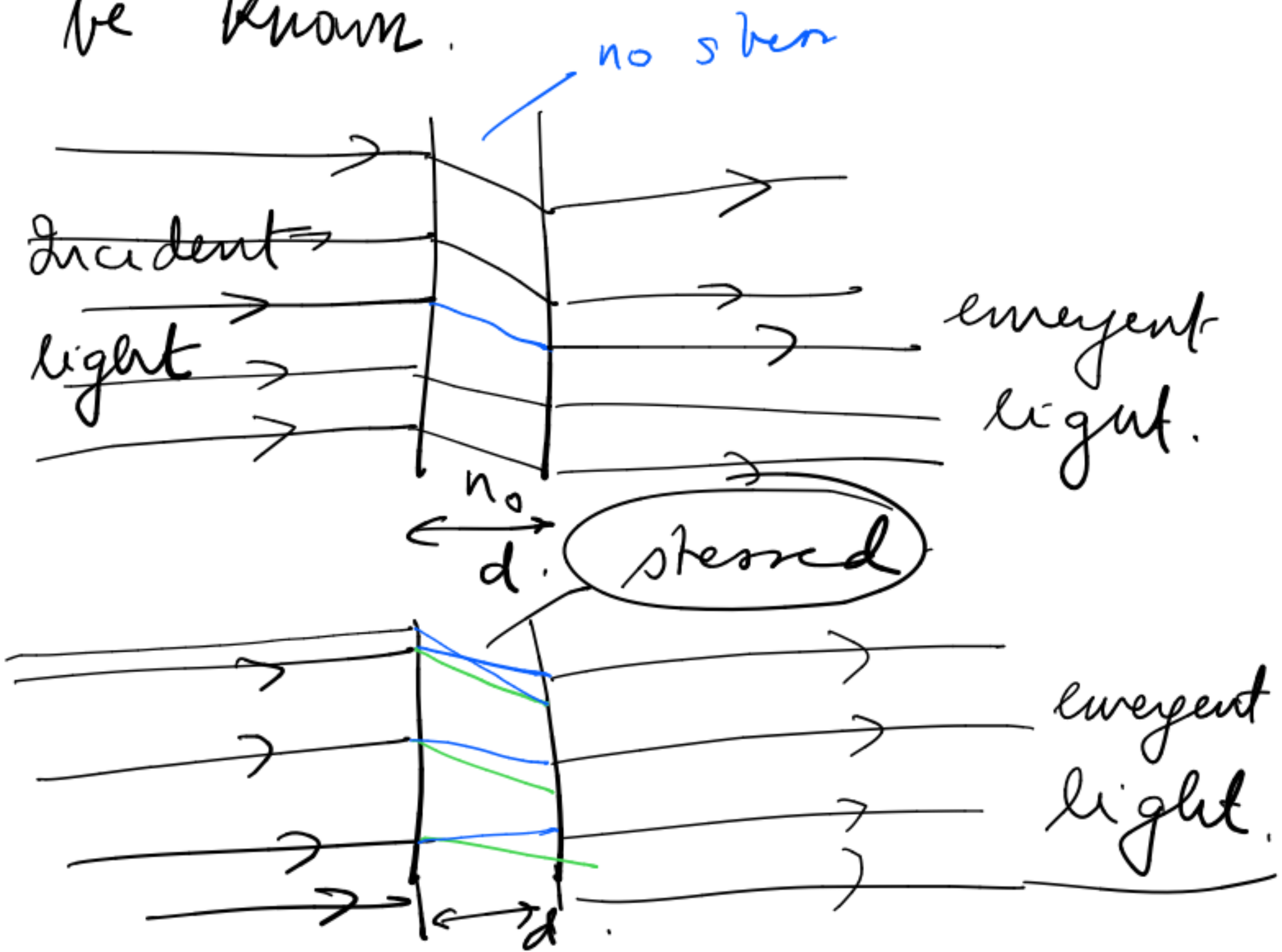
$$n_1 - n_3 = (\sigma_3 - \sigma_1) (c_2 - c_1)$$

→ (3)



If σ_1, σ_2 & principal directions
were known, then α is
also known.

But to fully characterize
birefringence of the loaded
plastic sheet Δ must also
be known.



The differently polarised light beams @ each point travel @ different speeds.

$$\parallel^e \sigma_1 \longrightarrow v_1$$

$$\parallel \sigma_2 \longrightarrow v_2.$$

time difference to travel through the sheet of thickness $d =$

$$t_2 - t_1 = \frac{d}{v_2} - \frac{d}{v_1}$$

$$= \frac{d}{c} \left\{ \frac{c}{v_2} - \frac{c}{v_1} \right\}$$

$$t_2 - t_1 = \frac{d}{c} (n_2 - n_1).$$

The phase lag corresponding to this time lag is:

$$\Delta = \frac{2\pi}{\lambda} c (t_2 - t_1)$$

$$= \frac{2\pi}{\lambda} \cancel{c} \frac{d}{\cancel{c}} (n_2 - n_1)$$

$$\Delta = \frac{2\pi}{\lambda} d (n_2 - n_1)$$

(4)

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- Incident light is phase shifted by $D = \frac{2\pi}{\lambda} d(n_2 - n_1)$ during passage thru' the loaded artificially birefr. plate of thickness d .

- $$n_2 - n_1 = (\sigma_1 - \sigma_2) \underset{\substack{\uparrow \\ c_2 - c_1}}{B} \quad \text{⊗}$$

B is called relative stress optic coefficient.

B is measured in Brewsters
1 Brewster = $10^{-6} / \text{MPa}$.

From (6):

$$\sigma_1 - \sigma_2 = f_{\sigma} \frac{\Delta}{2\pi d}, \quad (7)$$

\uparrow

$$\frac{\lambda}{B}$$

If we can measure Δ , we can find out $\sigma_1 - \sigma_2$.

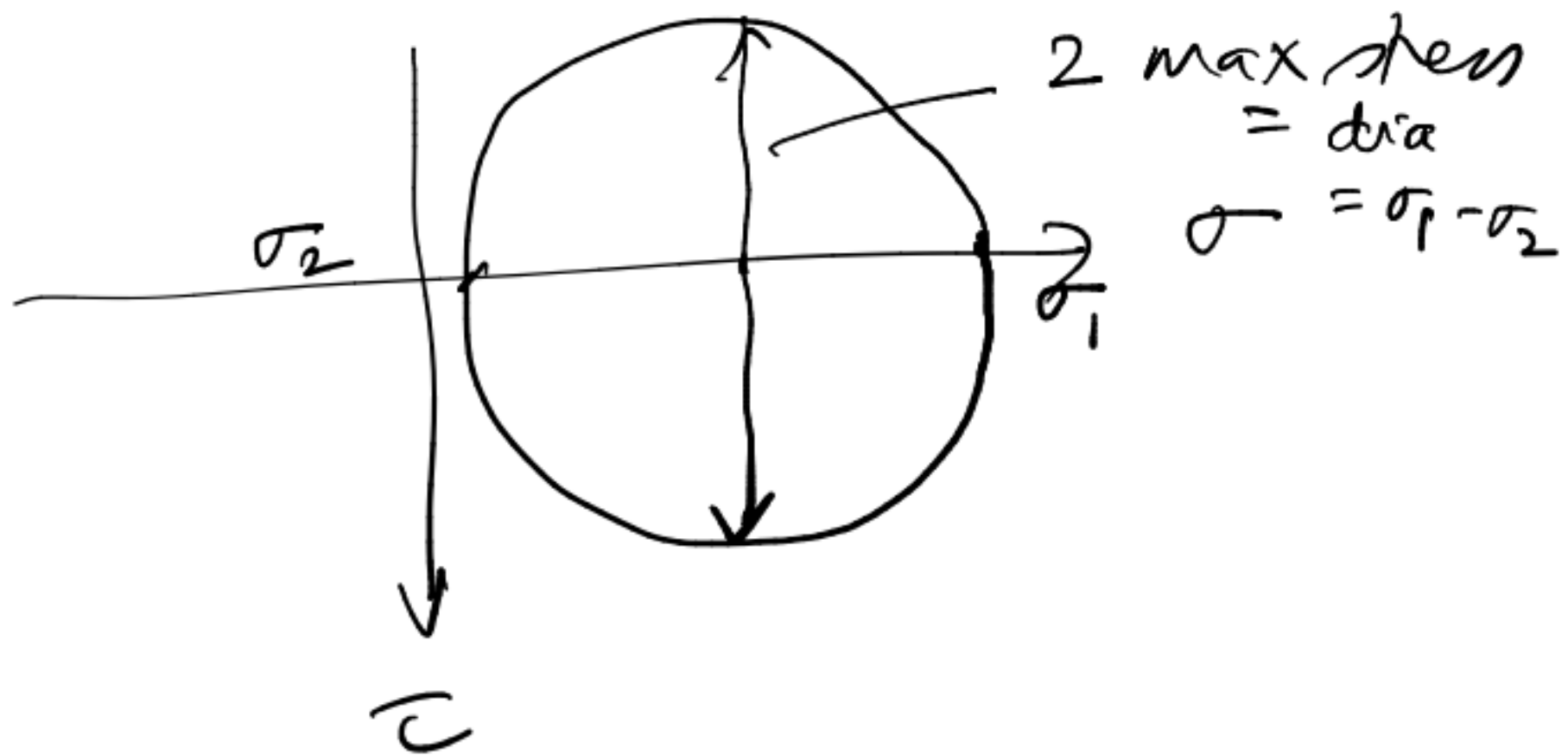
Using Hooke's law for plane σ_1 ,

$$\varepsilon_1 = \frac{1}{E} (\sigma_1 - \nu \sigma_2)$$

$$\varepsilon_2 = \frac{1}{E} (\sigma_2 - \nu \sigma_1)$$

$$\varepsilon_1 - \varepsilon_2 = \frac{1+\nu}{E} (\sigma_1 - \sigma_2) =$$

$$f_{\varepsilon} = \frac{1+\nu}{E} f_{\sigma} = f_{\varepsilon} \frac{\Delta}{2\pi d}, \quad \text{where}$$



$\sigma_1 - \sigma_2 = 2 \times \text{max shear}$
stress developed
at the point of
interest.

failure theories Tresca, & Mises
use the max. shear stress.

Polariscope : Tool to measure Δ .

Circular polariscope :

Works of circularly polarised light.

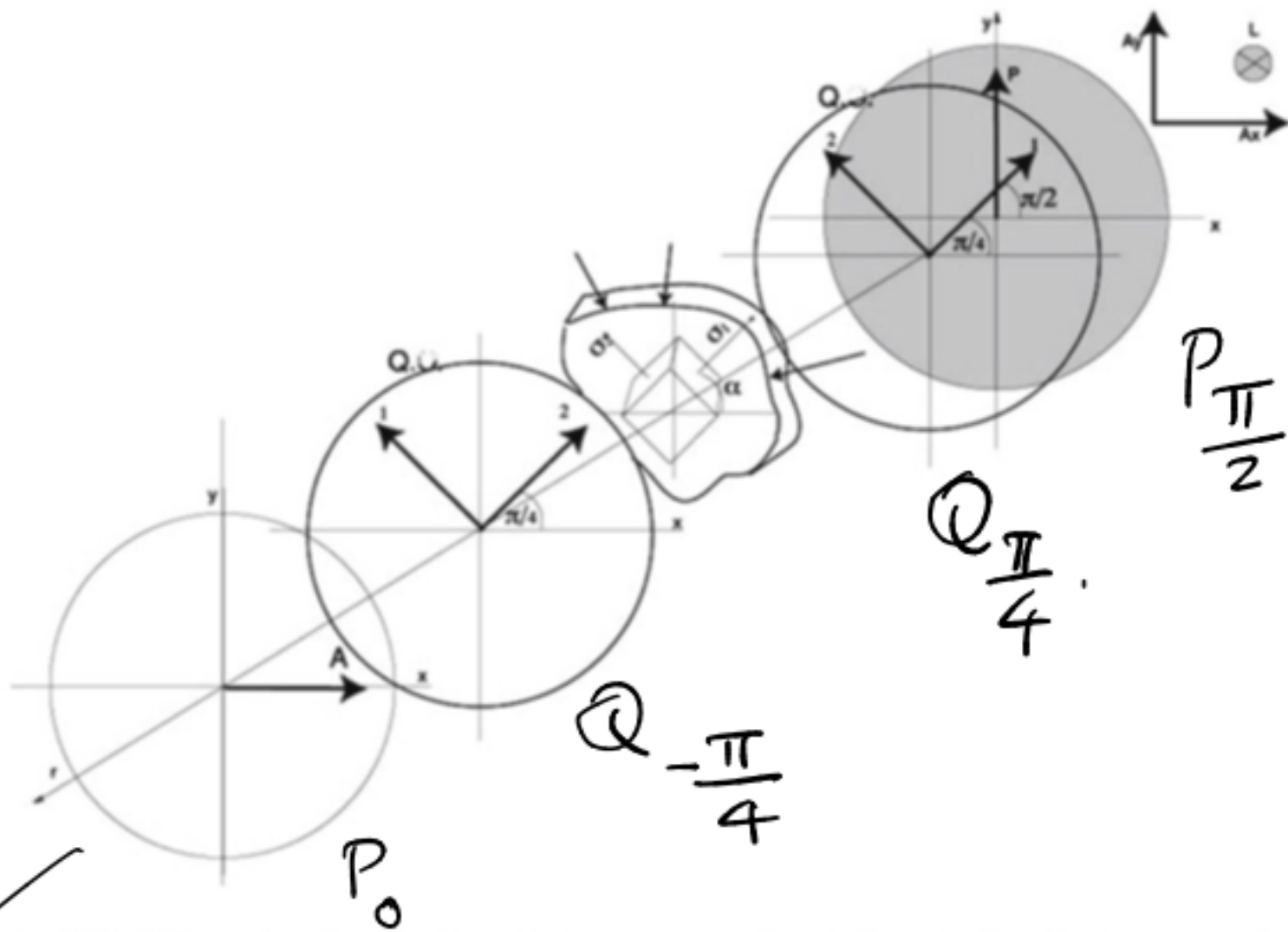


Fig. 3.11 Filters set-up in a circular polariscope: source L, polarizer P with axis along y, quarter-wave plate Q with axes 1 and 2 at $\pi/4$ and $3/4\pi$ respectively, plane model, second quarter-wave Q with axes 2 and 1 at $\pi/4$ and $3/4\pi$ respectively, analyzer A with its axis along x. Positive direction counterclockwise looking towards the light-source

photographic film.

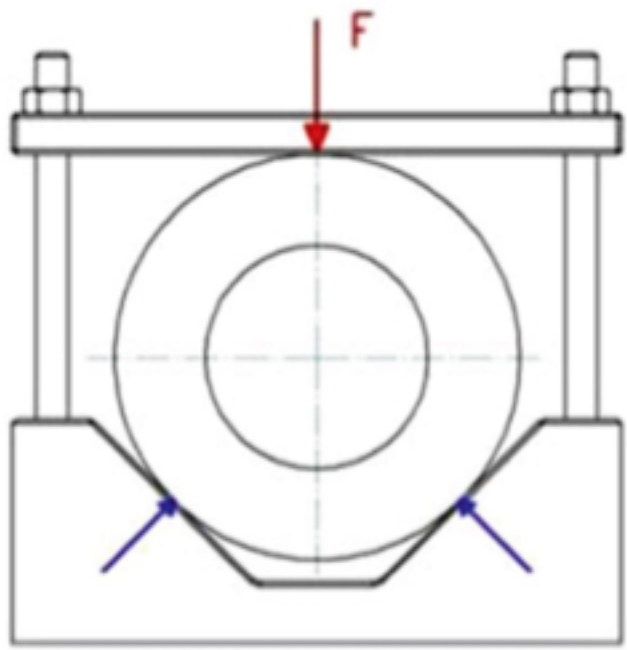


Fig. 3.12 Isochromatics on a black and bright background of an annular disc loaded at three points

Let the wave from $L \otimes$ have complex amplitudes $\begin{pmatrix} A_x \\ A_y \end{pmatrix}$.

$$\begin{pmatrix} A_x \\ A_y \end{pmatrix} = P_0 \quad Q_{\frac{\pi}{4}} \quad M \quad Q_{\frac{\pi}{4}} \quad P_{\frac{\pi}{2}} \begin{pmatrix} A_x \\ A_y \end{pmatrix}$$

$$= \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix} \begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} \begin{pmatrix} 1 & -i \\ -i & 1 \end{pmatrix} \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} A_x \\ A_y \end{pmatrix}$$

$$A'_x = A_y (2m_{21} - i m_{11} + i m_{22})$$

We know from lecture 8

$$\begin{cases} m_{11} = \cos^2 \alpha + e^{i\Delta} \sin^2 \alpha \\ m_{22} = \sin^2 \alpha + e^{i\Delta} \cos^2 \alpha \\ m_{12} = m_{21} = (1 - e^{i\Delta}) \sin \alpha \cos \alpha \end{cases}$$

$$A'_x = A_y (1 - e^{i\Delta}) (\sin^2 \alpha - i \cos 2\alpha)$$

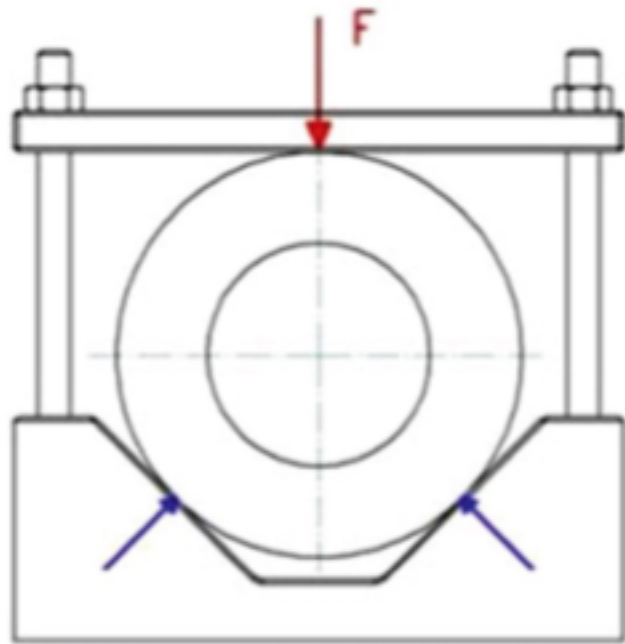
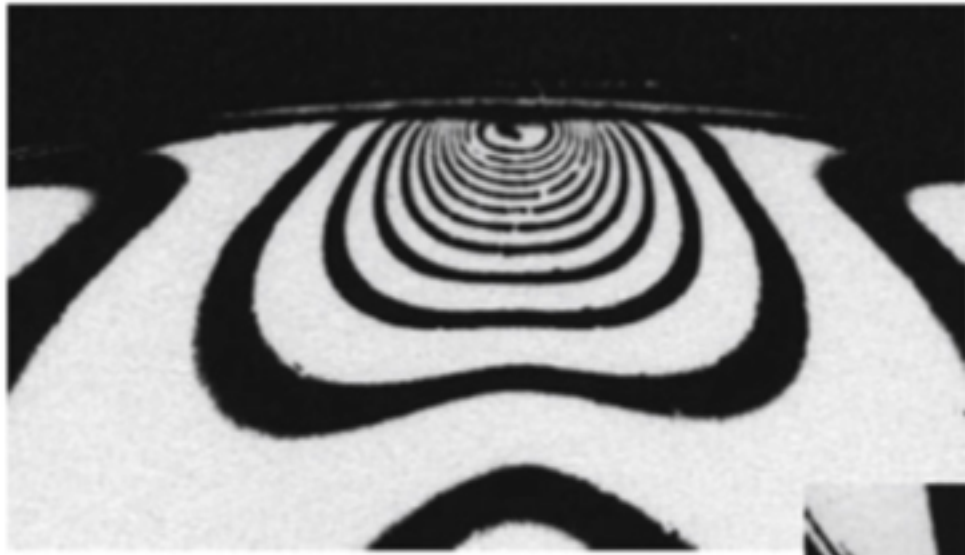


Fig. 3.12 Isochromatics on a black and bright background of an annular disc loaded at three points

In the regions that go dark in the film (dark fringes),

$$A'_x = 0$$



Monochromatic illumination.

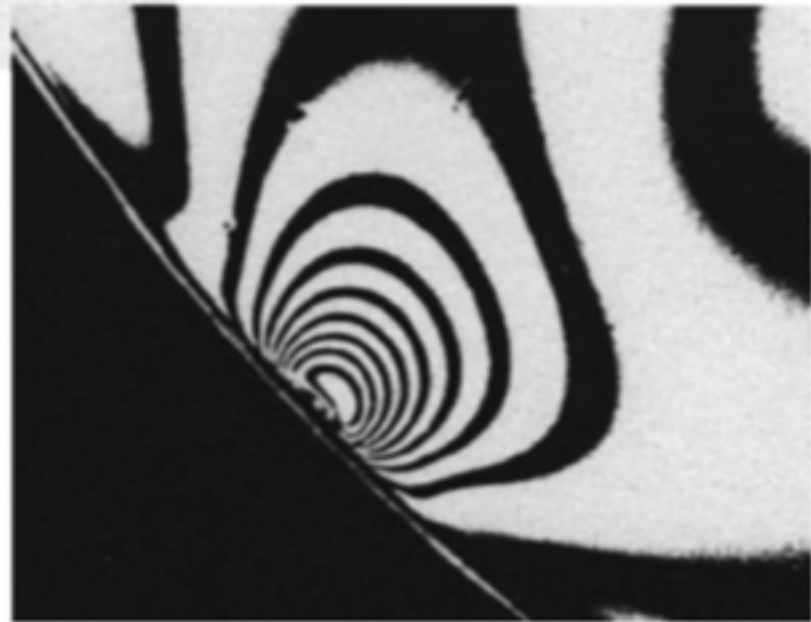
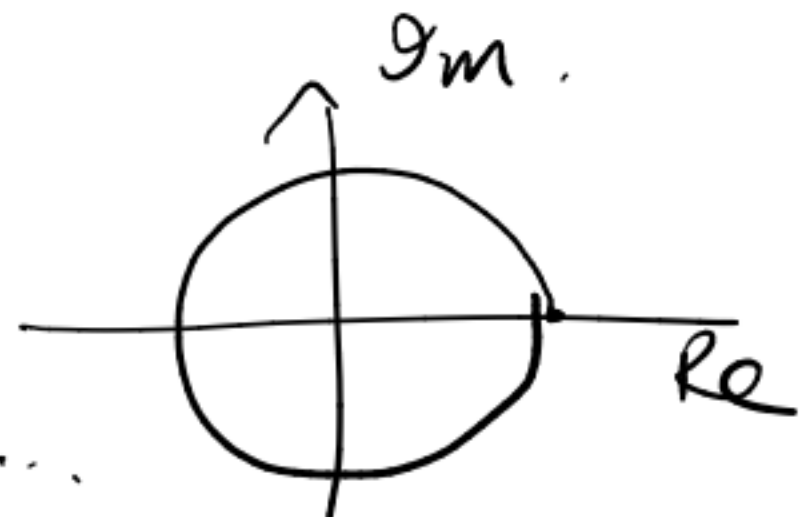


Fig. 3.13 Details of isochromatics in contact points without (up) and with a light friction (bottom)

Because $\sin 2\alpha - i \cos 2\alpha \neq 0$
 for any α , it follows
 that $1 - e^{i\Delta} = 0$ "extinction condition".

$$\Rightarrow e^{i\Delta} = 1.$$

Solution $\Rightarrow \frac{\Delta}{2\pi} = 0, 1, 2, \dots$



If white light were used instead of monochromatic light:

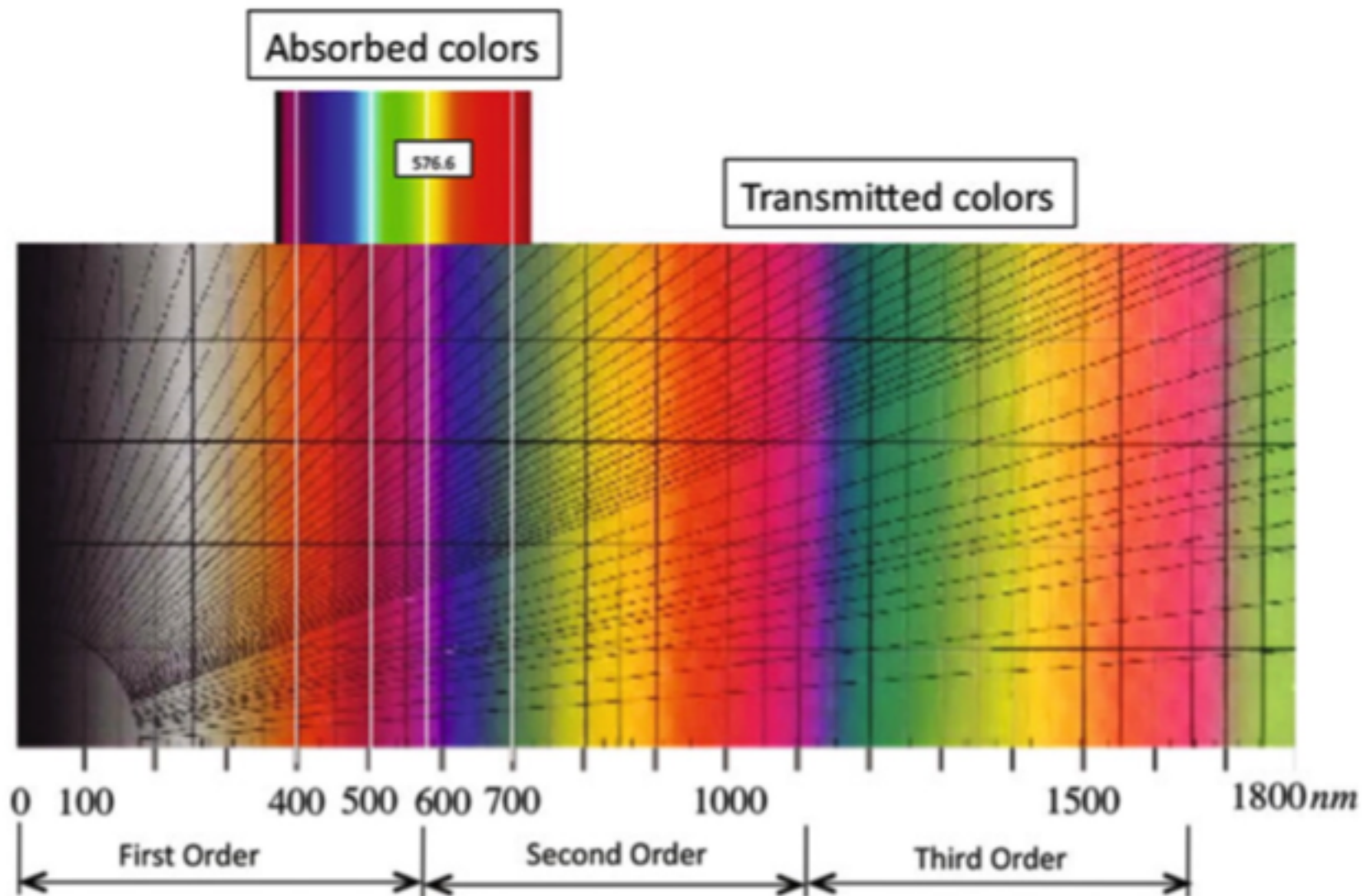


Fig. 3.14 Absorbed and transmitted color: modified from [16]

The colors that appear in the fringe pattern are those that were transmitted. Their complementary color was extinguished. \rightarrow Use this to find λ & Δ .

